TEXAS INSTRUMENTS



TAS5162

SLES194D-OCTOBER 2006-REVISED JULY 2007

# 2 x 210 Watt STEREO DIGITAL AMPLIFIER POWER STAGE

## FEATURES

- 2×160 W at 10% THD+N Into 8- $\Omega$  BTL
- 2×210 W at 10% THD+N Into 6-Ω BTL
- 1×300 W at 10% THD+N Into 4-Ω PBTL <sup>(1)</sup>
- >110 dB SNR (A-Weighted, TAS5518 Modulator)
- <0.09% THD+N at 1 W
- Two Thermally Enhanced Package Options:
  - DKD (36-pin PSOP3)
  - DDV (44-pin HTSSOP)
- High-Efficiency Power Stage (>90%) With 80-mΩ Output MOSFETs
- Power-On Reset for Protection on Power Up
  Without Any Power-Supply Sequencing
- Integrated Self-Protection Circuits Including Undervoltage, Overtemperature, Overload, Short Circuit
- Error Reporting
- EMI Compliant When Used With Recommended System Design
- Intelligent Gate Drive
- Mid-Z Ramp Compatible for reduced "pop noise"

## APPLICATIONS

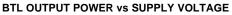
- Mini/Micro Audio System
- DVD Receiver
- Home Theater

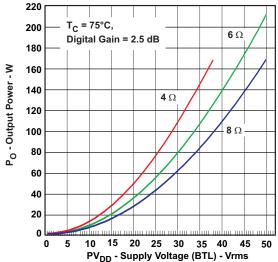
## DESCRIPTION

The TAS5162 is a high performance, integrated stereo digital amplifier power stage with an improved protection system. The TAS5162 is capable of driving a 6- $\Omega$  bridge-tied load (BTL) at up to 210 W per channel at THD = 10%, low integrated noise at the output, low THD+N performance without clipping, and low idle power dissipation.

A low-cost, high-fidelity audio system can be built using a TI chipset, comprising a modulator (e.g., TAS5508) and the TAS5162. This system only requires a simple passive LC demodulation filter to deliver high-quality, high-efficiency audio amplification with proven EMI compliance. This device requires two power supplies, at 12 V for GVDD and VDD, and at 50V for PVDD. The TAS5162 does not require power-up sequencing due to internal power-on reset. The efficiency of this digital amplifier is greater than 90% into 6  $\Omega$ , which enables the use of smaller power supplies and heatsinks.

The TAS5162 has an innovative protection system integrated on-chip, safeguarding the device against a wide range of fault conditions that could damage the safeguards system. These are short-circuit protection, overcurrent protection, undervoltage protection, and overtemperature protection. The TAS5162 has a new proprietary current-limiting circuit that reduces the possibility of device shutdown durina high-level music transients. А new programmable overcurrent detector allows the use of lower-cost inductors in the demodulation output filter.





(1) The DDV package will deliver the stated maximum power levels; however, this is dependant on system configuration. The smaller pad area also makes the thermal interface to the heatsink more important. For multichannel systems that require two channels to be driven at full power with the DDV package option, it is recommended to design the system so that the two channels are in two separate devices.

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## TAS5162

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These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

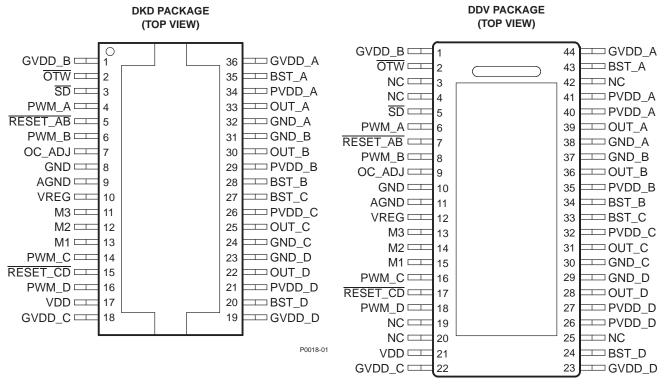
#### **GENERAL INFORMATION**

#### **Terminal Assignment**

The TAS5162 is available in two thermally enhanced packages:

- 36-pin PSOP3 package (DKD)
- 44-pin HTSSOP PowerPad<sup>™</sup> package (DDV)

Both package types contain a heat slug that is located on the top side of the device for convenient thermal coupling to the heatsink.



P0016-02

## **GENERAL INFORMATION (continued)**

### **MODE Selection Pins for Both Packages**

Ν	IODE PIN	IS	PWM INPUT		PROTECTION SCHEME
М3	M2	M1		OUTPUT CONFIGURATION	PROTECTION SCHEME
0	0	0	2N <sup>(1)</sup> AD/BD modulation	2 channels BTL output	BTL mode, full protection <sup>(2)</sup>
0	0	1	2N <sup>(1)</sup> AD/BD modulation	2 channels BTL output	BTL mode, latching shutdown <sup>(2)</sup>
0	1	0	1N <sup>(1)</sup> AD modulation	2 channels BTL output	BTL mode, full protection <sup>(2)</sup>
0	1	1	1N <sup>(1)</sup> AD modulation	1 channel PBTL output	PBTL mode, full protection. Only PWM_A input is used.
1	0	0	1N <sup>(1)</sup> AD modulation	4 channels SE output	Protection works similarly to BTL mode $^{(2)}$ . Only difference in SE mode is that OUT_X is Hi-Z instead of a pulldown through internal pulldown resistor.
1	0	1	1N <sup>(1)</sup> AD modulation	4 channels SE output - No PWM Input protection, latching shutdown	Protection works similarly to SE Mode <sup>(2)</sup> (1,0,0); however, the PWM input protection is disabled. Also, overcurrent detection will latch if an error occurs.
1	1	0	Decement		·
1	1	1	Reserved		

(1) The 1N and 2N naming convention is used to indicate the required number of PWM lines to the power stage per channel in a specific mode.

(2) An overload protection (OLP) occurring on A or B causes both channels to shut down. An OLP on C or D works similarly. Global errors like overtemperature error (OTE), undervoltage protection (UVP), and power-on reset (POR) affect all channels.

## Package Heat Dissipation Ratings<sup>(1)</sup>

PARAMETER	TAS5162DKD	TAS5162DDV
R <sub>0JC</sub> (°C/W)—2 BTL or 4 SE channels (8 transistors)	1.0	1.1
R <sub>0JC</sub> (°C/W)—1 BTL or 2 SE channel(s) (4 transistors)	1.5	2.2
R <sub>0JC</sub> (°C/W)—(1 transistor)	5.0	7.4
Pad area <sup>(2)</sup>	80 mm <sup>2</sup>	34 mm <sup>2</sup>

(1) JC is junction-to-case, CH is case-to-heatsink.

(2) R<sub>8CH</sub> is an important consideration. Assume a 2-mil thickness of typical thermal grease between the pad area and the heatsink and both channels active. The R<sub>8CH</sub> with this condition is 2.6°C/W for the DKD package and 4.0°C/W for the DDV package.

## **ABSOLUTE MAXIMUM RATINGS**

over operating free-air temperature range unless otherwise noted <sup>(1)</sup>

TAS5162	TAS5162			
VDD to AGND	–0.3 V to 13.2 V			
GVDD_X to AGND	–0.3 V to 13.2 V			
PVDD_X to GND_X <sup>(2)</sup>	-0.3 V to 71 V			
OUT_X to GND_X <sup>(2)</sup>	-0.3 V to 71V			
BST_X to GND_X <sup>(2)</sup>	–0.3 V to 79.7 V			
VREG to AGND	–0.3 V to 4.2 V			
GND_X to GND	–0.3 V to 0.3 V			
GND_X to AGND	–0.3 V to 0.3 V			
GND to AGND	–0.3 V to 0.3 V			
PWM_X, OC_ADJ, M1, M2, M3 to AGND	–0.3 V to 4.2 V			
RESET_X, SD, OTW to AGND	–0.3 V to 7 V			
Maximum continuous sink current (SD, OTW)	9 mA			
Maximum operating junction temperature range, T <sub>J</sub>	0°C to 125°C			
Storage temperature	-40°C to 125°C			
Lead temperature, 1,6 mm (1/16 inch) from case for 10 seconds	260°C			
Minimum pulse duration, low	50 ns			

(1) Stresses beyond those listed under "absolute maximum ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under "recommended operating conditions" is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

(2) These voltages represent the dc voltage + peak ac waveform measured at the terminal of the device in all conditions.

## ORDERING INFORMATION

T <sub>A</sub>	PACKAGE	DESCRIPTION
0°C to 70°C	TAS5162DKD	36-pin PSOP3
0°C to 70°C	TAS5162DDV	44-pin HTSSOP

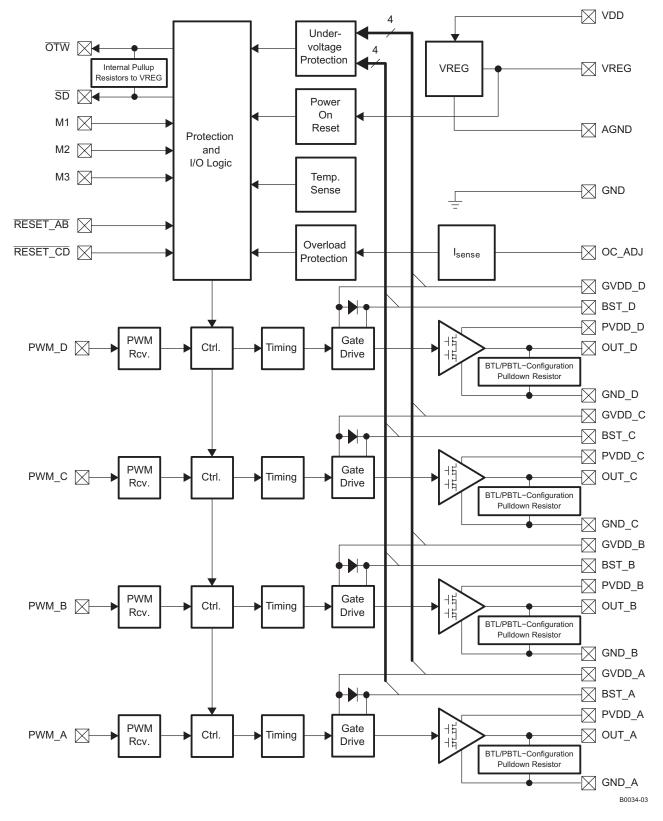
For the most current specification and package information, see the TI Web site at www.ti.com.

## **Terminal Functions**

TERMINAL		FUNCTION <sup>(1)</sup>	1) DESCRIPTION		
NAME	DKD NO.	DDV NO.	FUNCTION	DESCRIPTION	
AGND	9	11	Р	Analog ground	
BST_A	35	43	Р	HS bootstrap supply (BST), external .033- $\mu$ F capacitor to OUT_A required	
BST_B	28	34	Р	HS bootstrap supply (BST), external .033- $\mu$ F capacitor to OUT_B required	
BST_C	27	33	P HS bootstrap supply (BST), external .033-μF capacito required		
BST_D	20	24	Р	HS bootstrap supply (BST), external .033-µF capacitor to OUT_D required	
GND	8	10	Р	Ground	
GND_A	32	38	Р	Power ground for half-bridge A	
GND_B	31	37	Р	Power ground for half-bridge B	
GND_C	24	30	Р	Power ground for half-bridge C	
GND_D	23	29	Р	Power ground for half-bridge D	
GVDD_A	36	44	Р	Gate-drive voltage supply requires 0.1-µF capacitor to AGND	
GVDD_B	1	1	Р	Gate-drive voltage supply requires 0.1-µF capacitor to AGND	
GVDD_C	18	22	Р	Gate-drive voltage supply requires 0.1-µF capacitor to AGND	
GVDD_D	19	23	Р	Gate-drive voltage supply requires 0.1-µF capacitor to AGND	
M1	13	15	1	Mode selection pin	
M2	12	14	1	Mode selection pin	
M3	11	13		Mode selection pin	
NC		3, 4, 19, 20, 25, 42		No connect. Pins may be grounded.	
OC_ADJ	7	9	0	Analog overcurrent programming pin requires resistor to ground	
OTW	2	2	0	Overtemperature warning signal, open-drain, active-low	
OUT_A	33	39	0	Output, half-bridge A	
OUT_B	30	36	0	Output, half-bridge B	
OUT_C	25	31	0	Output, half-bridge C	
OUT_D	22	28	0	Output, half-bridge D	
PVDD_A	34	40, 41	Р	Power supply input for half-bridge A requires close decoupling of $0.01$ - $\mu$ F capacitor in parallel with a $1.0$ - $\mu$ F capacitor to GND_A.	
PVDD_B	29	35	Р	Power supply input for half-bridge B requires close decoupling of $0.01$ - $\mu$ F capacitor in parallel with a $1.0$ - $\mu$ F capacitor to GND_B.	
PVDD_C	26	32	Р	Power supply input for half-bridge C requires close decoupling of $0.01$ - $\mu$ F capacitor in parallel with a $1.0$ - $\mu$ F capacitor to GND_C.	
PVDD_D	21	26, 27	Р	Power supply input for half-bridge D requires close decoupling of $0.01$ - $\mu$ F capacitor in parallel with a 1.0- $\mu$ F capacitor to GND_D.	
PWM_A	4	6	I	Input signal for half-bridge A	
PWM_B	6	8	I	Input signal for half-bridge B	
PWM_C	14	16	I	Input signal for half-bridge C	
PWM_D	16	18	I	Input signal for half-bridge D	
RESET_AB	5	7	I	Reset signal for half-bridge A and half-bridge B, active-low	
RESET_CD	15	17	I	Reset signal for half-bridge C and half-bridge D, active-low	
SD	3	5	0	Shutdown signal, open-drain, active-low	
VDD	17	21	P	Power supply for digital voltage regulator requires a $47-\mu F$ capacitor in parallel with a $0.1-\mu F$ capacitor to GND for decoupling	
VREG	10	12	Р	Digital regulator supply filter pin requires 0.1-µF capacitor to AGND.	

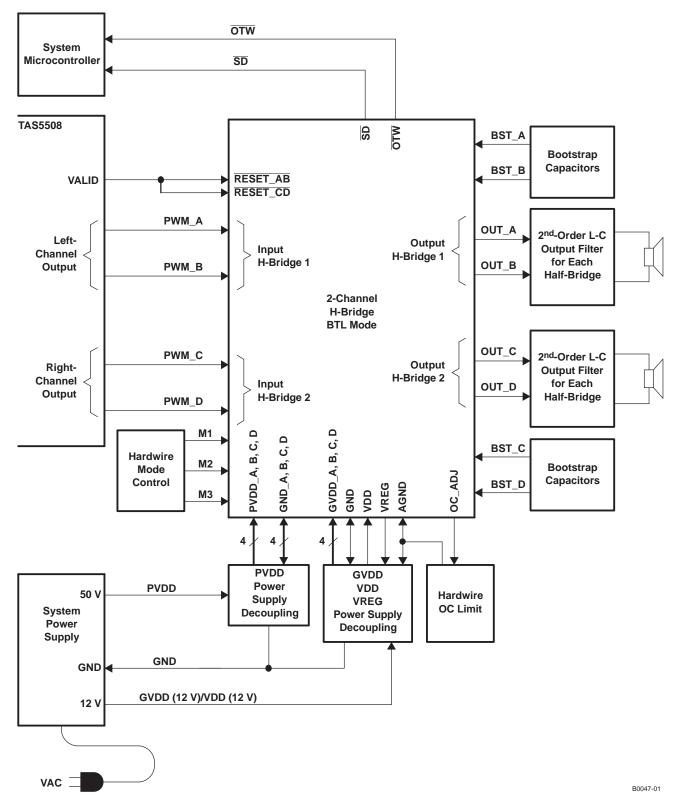
(1) I = input, O = output, P = power

## SYSTEM BLOCK DIAGRAM





## FUNCTIONAL BLOCK DIAGRAM



## **RECOMMENDED OPERATING CONDITIONS**

			MIN	TYP	MAX	UNIT
PVDD_X	Half-bridge supply	DC supply voltage	0	50	52.5	V
GVDD_X	Supply for logic regulators and gate-drive circuitry	DC supply voltage	10.8	12	13.2	V
VDD	Digital regulator input	DC supply voltage	10.8	12	13.2	V
R <sub>L</sub> (BTL)		Output filter: $L = 10 \mu H$ , $C = 470 nF$ .	4.6	6-8		
R <sub>L</sub> (SE)	Load impedance	Output AD modulation, switching	2.5	3-8		Ω
R <sub>L</sub> (PBTL)		frequency > 350 kHz		4-8		
L <sub>Output</sub> (BTL)			5	10		
L <sub>Output</sub> (SE)	Output-filter inductance	Minimum output inductance under short-circuit condition	5	10		μH
L <sub>Output</sub> (PBTL)	_		5	10		
F <sub>PWM</sub>	PWM frame rate		192	384	432	kHz
TJ	Junction temperature		0		125	°C

## AUDIO SPECIFICATIONS (BTL)

 $PVDD_X = 50 V$ , GVDD = VDD = 12 V, BTL mode,  $R_L = 6 \Omega$ ,  $R_{OC} = 22 K\Omega$ , audio frequency = 1 kHz, AES17 filter,  $F_{PWM} = 384$  kHz, case temperature = 75°C, unless otherwise noted. Audio performance is recorded as a chipset, using TAS5508 PWM processor with an effective modulation index limit of 96.1%. All performance is in accordance with recommended operating conditions unless otherwise specified.

PARAMETER		TEST CONDITIONS	TAS5162			UNIT	
	PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT	
		$R_L = 4 \Omega$ , 10% THD, clipped input signal (PVDD = 38.5 Volts)		160			
		$R_L = 6 \Omega$ , 10% THD, clipped input signal		210			
	Power output per channel, DKD package	$R_{L} = 8 \Omega$ , 10% THD, clipped input signal		160		W	
Po	Power output per channer, DRD package	$R_L = 4 \Omega$ , 0 dBFS, unclipped input signal (PVDD = 38.5 Volts)		120			
		$R_L = 6 \Omega$ , 0 dBFS, unclipped input signal		165			
		$R_L = 8 \Omega$ , 0 dBFS, unclipped input signal		125			
THD+N	Total harmonic distortion + poise	0 dBFS		0.2%			
	Total harmonic distortion + noise	1 W		0.09%			
V <sub>n</sub>	Output integrated noise	A-weighted, TAS5508 Modulator		140		μV	
		A-Weighted, TAS5518 Modulator		85			
SNR	Signal-to-noise ratio <sup>(1)</sup>	A-weighted, TAS5508 Modulator		102			
		A-weighted, TAS5518 Modulator		112		dB	
	Dynamic range	A-weighted, input level = -60 dBFS using TAS5508 modulator	102			٩D	
DNR		A-weighted, input level = -60 dBFS using TAS5518 modulator		112		dB	
P <sub>idle</sub>	Power dissipation due to idle losses (IPVDD_X)	$P_0 = 0$ W, 4 channels switching <sup>(2)</sup>		2.5		W	

(1) SNR is calculated relative to 0-dBFS input level.

(2) Actual system idle losses are affected by core losses of output inductors.

## AUDIO SPECIFICATIONS (Single-Ended Output)

 $PVDD_X = 50 V$ , GVDD = VDD = 12 V, SE mode,  $R_L = 3 \Omega$ ,  $R_{OC} = 22 K\Omega$ , audio frequency = 1 kHz, AES17 filter,  $F_{PWM} = 384$  kHz, case temperature = 75°C, unless otherwise noted. Audio performance is recorded as a chipset, using TAS5086 PWM processor with an effective modulation index limit of 96.1%. All performance is in accordance with recommended

## AUDIO SPECIFICATIONS (Single-Ended Output) (continued)

 $PVDD_X = 50 V$ , GVDD = VDD = 12 V, SE mode,  $R_L = 3 \Omega$ ,  $R_{OC} = 22 K\Omega$ , audio frequency = 1 kHz, AES17 filter,  $F_{PWM} = 384$  kHz, case temperature = 75°C, unless otherwise noted. Audio performance is recorded as a chipset, using TAS5086 PWM processor with an effective modulation index limit of 96.1%. All performance is in accordance with recommended operating conditions unless otherwise specified.

operating conditions unless otherwise specified.

	DADAMETED		Т			
	PARAMETER	TEST CONDITIONS	MIN	MIN TYP MAX		UNIT
Po		$R_L = 3 \Omega$ , 10% THD, clipped input signal		105		
	Power output per channel, DKD package	$R_L = 4 \Omega$ , 10% THD, clipped input signal		80		W
	Power output per channel, DND package	$R_L = 3 \Omega$ , 0 dBFS, unclipped input signal	80		vv	
		$R_L = 4 \Omega$ , 0 dBFS, unclipped input signal	60			
	Total harmonic distortion + noise	0 dBFS		0.2%		
THD+N	Total harmonic distortion + noise	1 W		0.09%		
V <sub>n</sub>	Output integrated noise	A-weighted		85		μV
SNR	Signal-to-noise ratio <sup>(1)</sup>	A-weighted		110		dB
DNR	Dynamic range	A-weighted, input level = -60 dBFS using TAS5086 modulator		110		dB
P <sub>idle</sub>	Power dissipation due to idle losses (IPVDD_X)	$P_O = 0$ W, 4 channels switching <sup>(2)</sup>		2.5		W

(1) SNR is calculated relative to 0-dBFS input level.

(2) Actual system idle losses are affected by core losses of output inductors.

## AUDIO SPECIFICATIONS (PBTL)

 $PVDD_X = 50 V$ , GVDD = VDD = 12 V, PBTL mode,  $R_L = 4\Omega$ ,  $R_{OC} = 22 K\Omega$ , 1/2 of an MBRM5100-13 dual, 5A@100V, Schottky diode connected from each output pin to to ground, audio frequency = 1 kHz, AES17 filter,  $F_{PWM} = 384$  kHz, case temperature = 75°C, unless otherwise noted. Audio performance is recorded as a chipset, using TAS5508 PWM processor with an effective modulation index limit of 96.1%. All performance is in accordance with recommended operating conditions unless otherwise specified.

	DADAMETED	TEST CONDITIONS	T.				
	PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT	
Po		$R_L = 4 \Omega$ , 10% THD, clipped input signal		300			
	Dower output per channel, DKD perform	$R_L = 4 \Omega$ , 0 dBFS, unclipped input signal		240		14/	
	Power output per channel, DKD package	$R_L = 3 \Omega$ , 10% THD, clipped input signal		400		W	
		$R_L = 3 \Omega$ , 0 dBFS, unclipped input signal		300			
	Total harmonia distortion + pains	0 dBFS		0.2%			
THD+N	Total harmonic distortion + noise	1 W		0.09%			
V <sub>n</sub>	Output integrated noise	A-weighted		140		μV	
SNR	Signal-to-noise ratio <sup>(1)</sup>	A-weighted		102		dB	
DNR	Dynamic range	A-weighted, input level = -60 dBFS using TAS5508 modulator		102		٩D	
		A-weighted, input level = -60 dBFS using TAS5518 modulator		110		dB	
P <sub>idle</sub>	Power dissipation due to idle losses (IPVDD_X)	$P_0 = 0$ W, 1 channel switching <sup>(2)</sup>		2.5		W	

(1) SNR is calculated relative to 0-dBFS input level.

(2) Actual system idle losses are affected by core losses of output inductors.

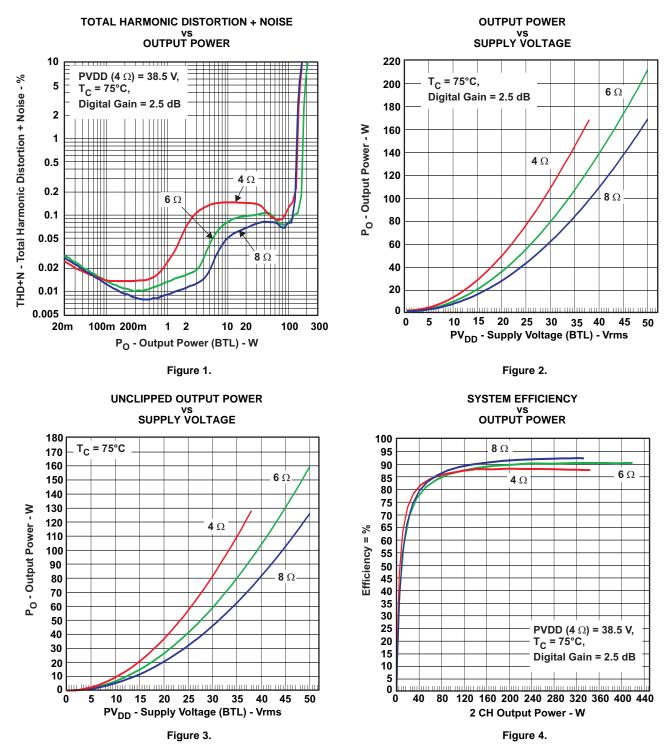
## **ELECTRICAL CHARACTERISTICS**

 $R_L$ = 6  $\Omega$ ,  $F_{PWM}$  = 384 kHz, unless otherwise noted. All performance is in accordance with recommended operating conditions unless otherwise specified.

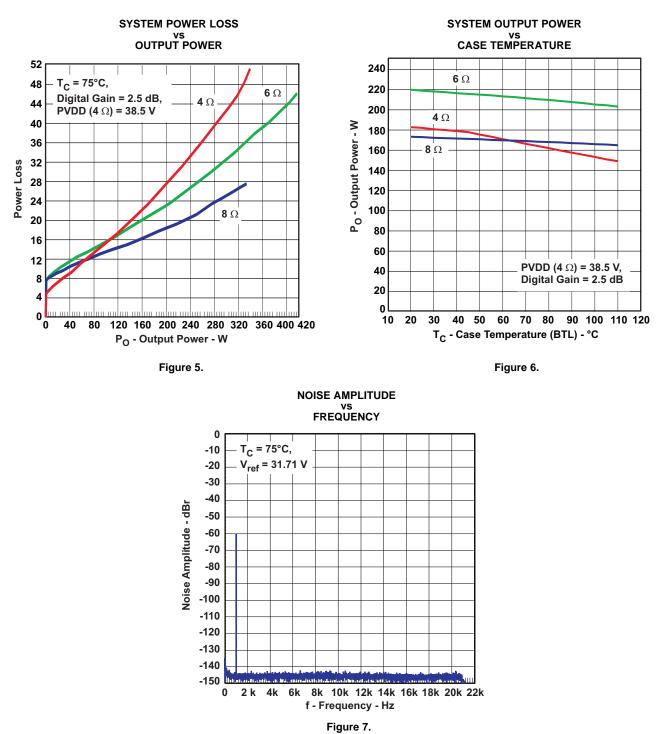
	PARAMETER	TEST CONDITIONS	<b>T</b> /	AS5162		UNIT
	FARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
Internal Voltage	e Regulator and Current Consumption	I.				
VREG	Voltage regulator, only used as a reference node	VDD = 12 V	2.95	3.3	3.65	V
		Operating, 50% duty cycle		10		
IVDD	VDD supply current	Idle, reset mode		6		mA
IGVDD_X	Coto oupply ourrent per helf bridge	50% duty cycle		8		mA
IGVDD_X	Gate supply current per half-bridge	Reset mode		0.3		IIIA
IPVDD_X	Half-bridge idle current	50% duty cycle, without output filter or load		15		mA
		Reset mode, no switching		500		μA
Output Stage M	IOSFETs					
R <sub>DSon,LS</sub>	Drain-to-source resistance, LS	$T_J = 25^{\circ}$ C, includes metallization resistance, GVDD = 12 V		90		mΩ
R <sub>DSon,HS</sub>	Drain-to-source resistance, HS	$T_J = 25^{\circ}$ C, includes metallization resistance, GVDD = 12 V		90		mΩ
I/O Protection						
V <sub>uvp,G</sub>	Undervoltage protection limit, GVDD_X			8.5		V
V <sub>uvp,hyst</sub> <sup>(1)</sup>				400		mV
OTW <sup>(1)</sup>	Overtemperature warning		115	125	135	°C
OTW <sub>HYST</sub> <sup>(1)</sup>	Temperature drop needed below OTW temp. for OTW to be inactive after the OTW event			25		°C
OTE <sup>(1)</sup>	Overtemperature error		145	155	165	°C
OTE- OTW <sub>differential</sub> <sup>(1)</sup>	OTE-OTW differential			25		°C
OTE <sub>HYST</sub> <sup>(1)</sup>	A reset needs to occur for $\overline{SD}$ for be released following an OTE event.			25		°C
OLPC	Overload protection counter	F <sub>PWM</sub> = 384 kHz		1.3		ms
I <sub>OC</sub>	Overcurrent limit protection	Resistor—programmable, nominal, $R_{OCP} = 22 \ k\Omega$		12		А
I <sub>OCT</sub>	Overcurrent response time	Time from application of short condition to Hi-Z of affected 1/2 bridge		250		ns
R <sub>OCP</sub>	OC programming resistor range	Resistor tolerance = 5%	22		69	kΩ
R <sub>PD</sub>	Internal pulldown resistor at the output of each half-bridge	Connected when RESET is active to provide bootstrap capacitor charge. Not used in SE mode		1.0		kΩ
Static Digital Sp	pecifications					
V <sub>IH</sub>	High-level input voltage	PWM_A, PWM_B, PWM_C, PWM_D, M1,	2			V
V <sub>IL</sub>	Low-level input voltage	M2, M3, RESET_AB, RESET_CD			0.8	V
Leakage	Input leakage current		-100		100	μA
OTW/SHUTDOV	VN (SD)					
R <sub>INT_PU</sub>	Internal pullup resistance, OTW to VREG, SD to VREG		20	26	35	kΩ
M		Internal pullup resistor	2.95	3.3	3.65	V
V <sub>OH</sub>	High-level output voltage	External pullup of 4.7 $k\Omega$ to 5 V	4.5		5	V
V <sub>OL</sub>	Low-level output voltage	I <sub>O</sub> = 4 mA		0.2	0.4	V
FANOUT	Device fanout OTW, SD	No external pullup		30		Devices

(1) Specified by design





## **TYPICAL CHARACTERISTICS, BTL CONFIGURATION (continued)**





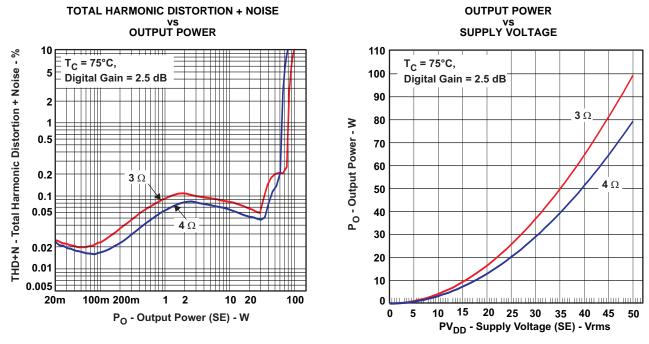


Figure 8.

120 110

100 90

20

P<sub>O</sub> - Output Power - W

3Ω

**4**Ω

Digital Gain = 2.5 dB

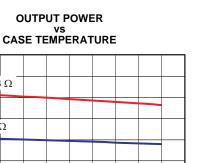


Figure 9.

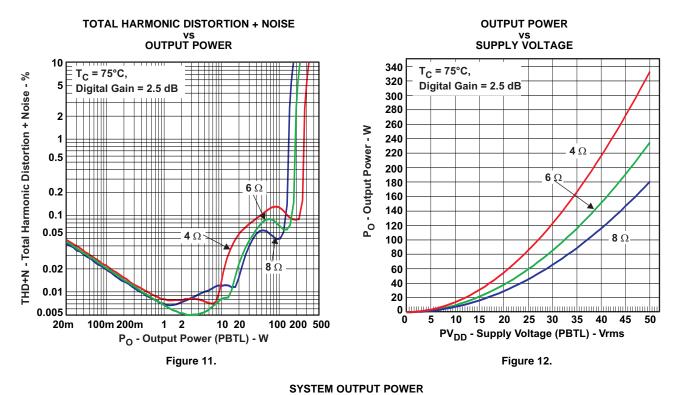
Figure 10.

T<sub>C</sub> - Case Temperature (SE) - °C

30 40 50 60 70 80 90 100 110 120



## **TYPICAL CHARACTERISTICS, PBTL CONFIGURATION**



vs CASE TEMPERATURE 4Ω 6Ω 8Ω

400 360

320

280

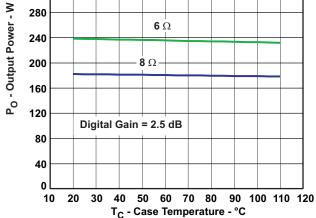


Figure 13.



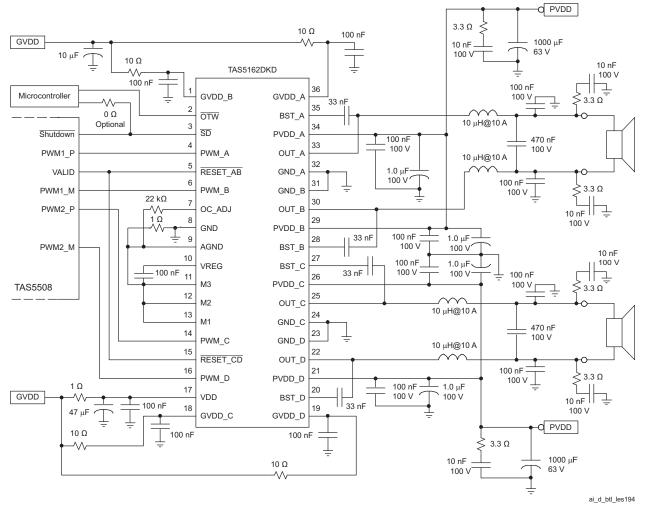


Figure 14. Typical Differential (2N) BTL Application With AD Modulation Filters (For Reference Only, component values and connection will change.)

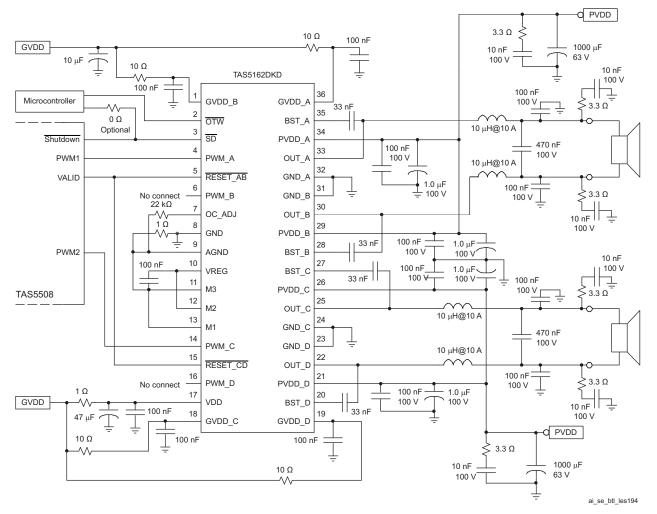


Figure 15. Typical Non-Differential (1N) BTL Application With AD Modulation Filters (For Reference Only, component values and connection will change.)

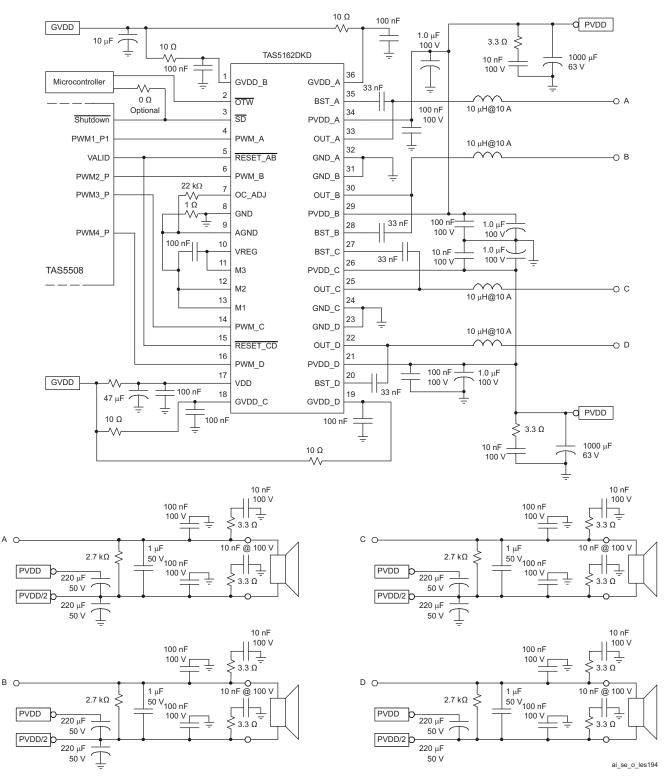
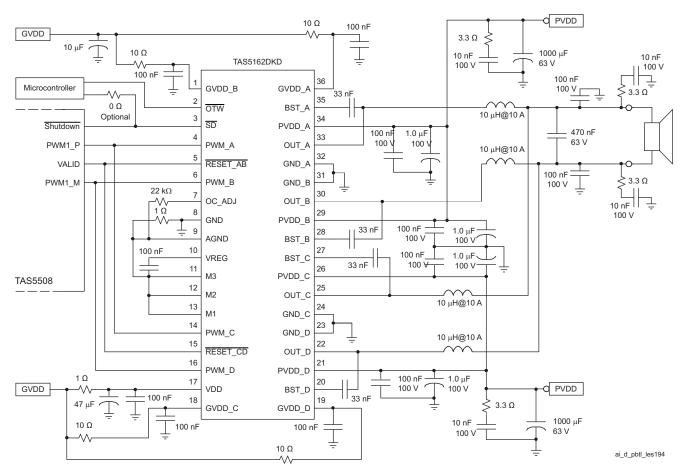


Figure 16. Typical SE Application (For Reference Only, component values and connection will change.)



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Figure 17. Typical Differential (2N) PBTL Application With AD Modulation Filters (For Reference Only, component values and connection will change.)

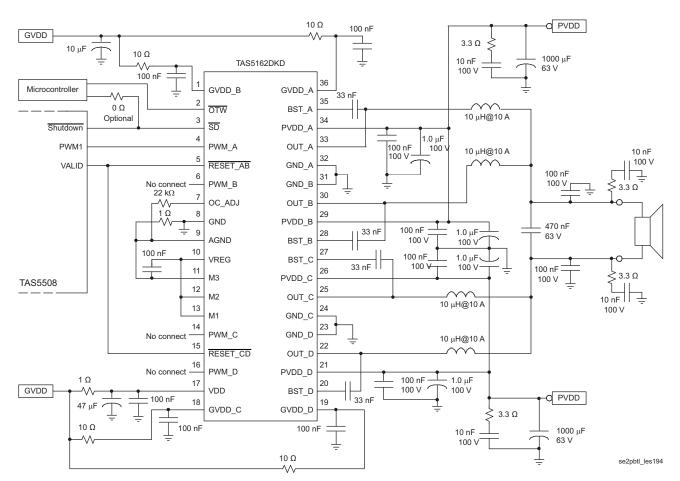


Figure 18. Typical Non-Differential (1N) PBTL Application (For Reference Only, component values and connection will change.)

## THEORY OF OPERATION

## **POWER SUPPLIES**

To facilitate system design, the TAS5162 needs only a 12-V supply in addition to the (typical) 50-V power-stage supply. An internal voltage regulator provides suitable voltage levels for the digital and low-voltage analog circuitry. Additionally, all circuitry requiring a floating voltage supply, e.g., the high-side gate drive, is accommodated by built-in bootstrap circuitry requiring only a few external capacitors.

In order to provide outstanding electrical and acoustical characteristics, the PWM signal path including gate drive and output stage is designed as identical, independent half-bridges. For this reason, each half-bridge has separate gate drive supply (GVDD\_X), bootstrap pins (BST\_X), and power-stage supply pins (PVDD X). Furthermore, an additional pin (VDD) is provided as supply for all common circuits. Although supplied from the same 12-V source, it is highly recommended to separate GVDD\_A, GVDD\_B, GVDD\_C, GVDD\_D, and VDD on the printed-circuit board (PCB) by RC filters (see application diagram for details). These RC filters provide the recommended high-frequency isolation. Special attention should be paid to placing all decoupling capacitors as close to their associated pins as possible. In general, inductance between the power supply pins and decoupling capacitors must be avoided. (See reference board documentation for additional information.)

For a properly functioning bootstrap circuit, a small ceramic capacitor must be connected from each bootstrap pin (BST\_X) to the power-stage output pin (OUT X). When the power-stage output is low, the bootstrap capacitor is charged through an internal diode connected between the gate-drive powersupply pin (GVDD\_X) and the bootstrap pin. When the power-stage output is high, the bootstrap capacitor potential is shifted above the output potential and thus provides a suitable voltage supply for the high-side gate driver. In an application with PWM switching frequencies in the range from 352 kHz to 384 kHz, it is recommended to use 33-nF ceramic capacitors, size 0603 or 0805, for the bootstrap supply. These 33-nF capacitors ensure sufficient energy storage, even during minimal PWM duty cycles, to keep the high-side power stage FET (LDMOS) fully turned on during the remaining part of the PWM cycle. In an application running at a reduced switching frequency, generally 192 kHz, the bootstrap capacitor might need to be increased in value.

Special attention should be paid to the power-stage power supply; this includes component selection, PCB placement, and routing. As indicated, each half-bridge has independent power-stage supply pins (PVDD\_X). For optimal electrical performance, EMI compliance, and system reliability, it is important that each PVDD\_X pin is decoupled with a 100-nF ceramic capacitor placed as close as possible to each supply pin. It is recommended to follow the PCB layout of the TAS5162 reference design. For additional information on recommended power supply and required components, see the application diagrams given previously in this data sheet.

The 12-V supply should be from a low-noise, low-output-impedance voltage regulator. Likewise, the 50-V power-stage supply is assumed to have low output impedance and low noise. The power-supply sequence is not critical as facilitated by the internal power-on-reset circuit. Moreover, the TAS5162 is fully protected against erroneous power-stage turn-on due to parasitic gate charging. Thus, voltage-supply ramp rates (dV/dt) are non-critical within the specified range (see the *Recommended Operating Conditions* section of this data sheet).

#### SYSTEM POWER-UP/POWER-DOWN SEQUENCE

### Powering Up

The TAS5162 does not require a power-up sequence. The outputs of the H-bridges remain in a highimpedance state until the gate-drive supply voltage (GVDD\_X) and VDD voltage are above the undervoltage protection (UVP) voltage threshold (see the *Electrical Characteristics* section of this data sheet). Although not specifically required, it is recommended to hold RESET\_AB and RESET\_CD in a low state while powering up the device. This allows an internal circuit to charge the external bootstrap capacitors by enabling a weak pulldown of the half-bridge output.

When the TAS5162 is being used with TI PWM modulators such as the TAS5508, no special attention to the state of RESET\_AB and RESET\_CD is required, provided that the chipset is configured as recommended.

#### **Powering Down**

The TAS5162 does not require a power-down sequence. The device remains fully operational as long as the gate-drive supply (GVDD\_X) voltage and VDD voltage are above the undervoltage protection (UVP) voltage threshold (see the *Electrical* 

*Characteristics* section of this data sheet). Although not specifically required, it is a good practice to hold RESET\_AB and RESET\_CD low during power down, thus preventing audible artifacts including pops or clicks.

When the TAS5162 is being used with TI PWM modulators such as the TAS5508, no special attention to the state of RESET\_AB and RESET\_CD is required, provided that the chipset is configured as recommended.

## Mid Z Sequence Compatibility

The TAS5162 is compatible with the Mid Z Sequence from the TAS5086 Modulator. The Mid Z Sequence is a series of pulses that is generated by the modulator that causes the power stage to slowly enable its outputs as it begins to switch.

By slowly starting the PWM switching, the impulse response created by the onset of switching is reduced. This impulse response is the acoustic artifact that is heard in the output transducers (loudspeakers) and is commonly termed a "click" or "pop".

The low acoustic artifact noise of TAS5162 will be further decreased when used in combination with a TAS5086 modulator and the Mid Z sequence is enabled.

The Mid Z Sequence is primarily used for the single-ended mode of operation. It facilitates a "softer" PWM output start after the split cap output configuration is charged.

## ERROR REPORTING

The SD and OTW pins are both active-low, open-drain outputs. Their function is for protection-mode signaling to a PWM controller or other system-control device.

Any fault resulting in device shutdown is signaled by the SD pin going low. Likewise, OTW goes low when the device junction temperature exceeds 125°C (see the following table).

SD	στω	DESCRIPTION
0	0	Overtemperature (OTE) or overload (OLP) or undervoltage (UVP)
0	1	Overload (OLP) or undervoltage (UVP)
1	0	Junction temperature higher than 125°C (overtemperature warning)
1	1	Junction temperature lower than 125°C and no OLP or UVP faults (normal operation)

Note that asserting either RESET\_AB or RESET\_CD low forces the SD signal high, independent of faults

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being present. TI recommends monitoring the OTW signal using the system microcontroller and responding to an overtemperature warning signal by, e.g., turning down the volume to prevent further heating of the device resulting in device shutdown (OTE).

To reduce external component count, an internal pullup resistor to 3.3 V is provided on both SD and OTW outputs. Level compliance for 5-V logic can be obtained by adding external pullup resistors to 5 V (see the *Electrical Characteristics* section of this data sheet for further specifications).

## **DEVICE PROTECTION SYSTEM**

The TAS5162 contains advanced protection circuitry carefully designed to facilitate system integration and ease of use, as well as to safeguard the device from permanent failure due to a wide range of fault conditions such as short circuits, overload, overtemperature, and undervoltage. The TAS5162 responds to a fault by immediately setting the power stage in a high-impedance (Hi-Z) state and asserting the SD pin low. In situations other than overload or over temperature, the device automatically recovers when the fault condition has been removed or the gate supply voltage has increased. For highest reliability, possible recovering from an overload/over-temperature fault requires external reset of the device (see the Device Reset section of this data sheet) no sooner than 1 second after the shutdown.

The TAS5162 contains circuitry associated with its PWM inputs that will detect the condition when a PWM input is continuously high or low. Without this protection circuitry, if a PWM input is not correct, the PVDD power supply could appear on the associated output pin. This condition could damage either the output load (loudspeaker) or the device. If a PWM input remains either high or low over  $15\mu$ S, the device's outputs will be set into a Hi-Z state. If this error condition occurs,  $\overline{SD}$  will not be asserted low.

The above mentioned operation is used for all of the BTL output modes except for Mode 0,0,1 and the Single-ended Mode 1,0,1 those are the Latching Shutdown Modes. In the Latching Shutdown Mode, the over current error recovery circuitry is disabled and an over current condition will cause the device to shutdown immediately. After shutdown, RESET\_AB and/or RESET\_CD must be asserted to restore normal operation after the over current condition is removed.

# Use of TAS5162 in High-Modulation-Index Capable Systems

This device requires at least 50 ns of low time on the output per 384-kHz PWM frame rate in order to keep the bootstrap capacitors charged. As an example, if the modulation index is set to 99.2% in the TAS5508. this setting allows PWM pulse durations down to 20 ns. This signal, which does not meet the 50-ns requirement, is sent to the PWM X pin and this low-state pulse time does not allow the bootstrap capacitor to stay charged. In this situation, the low voltage across the bootstrap capacitor can cause a failure of the high-side MOSFET transistor. especially when driving a low-impedance load. The TAS5162 device requires limiting the TAS5508 modulation index to less than 97.0% to keep the bootstrap capacitor charged under all signals and loads.

The device contains bootstrap capacitor under voltage protection circuit (BST\_UVP) that monitors the voltage on the bootstrap capacitors. When the voltage on the on the bootstrap capacitors is less than required for safe operation, the TAS5162 will initiate bootstrap capacitor recharge sequences until the bootstrap capacitors are properly charged for safe operation. This function may be activated at a modulation index of greater than 97.0%

TI strongly recommends using a TI PWM processor, such as TAS5508 or TAS5086, with the modulation index set at 96.1% to interface with TAS5162.

The Modulation Index is set by writing 0x04 to the Modulation Index Limit Register (0x16) in the TAS5508B or TAS5518A. In the case of the TAS5086 a 0x04 is written to the Modulation Limit Register (0x10).

# Overcurrent (OC) Protection With Current Limiting and Overload Detection

The device has independent, fast-reacting current detectors with programmable trip threshold (OC threshold) on all high-side and low-side power-stage FETs. See the following table for OC-adjust resistor values. The detector outputs are closely monitored by two protection systems. The first protection system controls the power stage in order to prevent the output current from further increasing, i.e., it performs a current-limiting function rather than prematurely shutting down during combinations of high-level music transients and extreme speaker load impedance drops. If the high-current situation persists, i.e., the power stage is being overloaded, a second protection system triggers a latching shutdown, resulting in the power stage being set in the high-impedance (Hi-Z) state. Current limiting and

overload protection are independent for half-bridges A and B and, respectively, C and D. That is, if the bridge-tied load between half-bridges A and B causes an overload fault, only half-bridges A and B are shut down.

- For the lowest-cost bill of materials in terms of component selection, the OC threshold measure should be limited, considering the power output requirement and minimum load impedance. Higher-impedance loads require a lower OC threshold.
- The demodulation-filter inductor must retain at least 5 µH of inductance at twice the OC threshold setting.

Unfortunately, most inductors have decreasing inductance with increasing temperature and increasing current (saturation). To some degree, an increase in temperature naturally occurs when operating at high output currents, due to core losses and the dc resistance of the inductor's copper winding. A thorough analysis of inductor saturation and thermal properties is strongly recommended.

Setting the OC threshold too low might cause issues such as lack of enough output power and/or unexpected shutdowns due to too-sensitive overload detection.

In general, it is recommended to follow closely the external component selection and PCB layout as given in the *Application* section.

added flexibility, the OC threshold For is programmable within a limited range using a single external resistor connected between the OC\_ADJ pin and AGND. (See the Electrical Characteristics section of this data sheet for information on the correlation between programming-resistor value and the OC threshold.) It should be noted that a properly functioning overcurrent detector assumes the presence of a properly designed demodulation filter at the power-stage output. Short-circuit protection is not provided directly at the output pins of the power stage but only on the speaker terminals (after the demodulation filter). It is required to follow certain guidelines when selecting the OC threshold and an appropriate demodulation inductor:

OC-Adjust Resistor Values (kΩ)	Max. Current Before OC Occurs (A)
22	12.2
27	10.5
47	6.4
68	4.0
100	3.0

### **Overtemperature Protection**

The TAS5162 has a two-level temperature-protection

system that asserts an active-low warning signal (OTW) when the device junction temperature exceeds 125°C (nominal) and, if the device junction temperature exceeds 155°C (nominal), the device is put into thermal shutdown, resulting in all half-bridge outputs being set in the high-impedance (Hi-Z) state and SD being asserted low. OTE is latched in this case and RESET\_AB and RESET\_CD must be asserted low.

# Undervoltage Protection (UVP) and Power-On Reset (POR)

The UVP and POR circuits of the TAS5162 fully protect the device in any power-up/down and brownout situation. While powering up, the POR circuit resets the overload circuit (OLP) and ensures that all circuits are fully operational when the GVDD\_X and VDD supply voltages reach 9.8 V (typical). Although GVDD\_X and VDD are independently monitored, a supply voltage drop below the UVP threshold on any VDD or GVDD\_X pin results in all half-bridge outputs immediately being set in the high-impedance (Hi-Z) state and SD being asserted low. The device automatically resumes operation when all supply voltage on the bootstrap capacitors have increased above the UVP threshold.

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#### DEVICE RESET

Two reset pins are provided for independent control of half-bridges A/B and C/D. When RESET\_AB is asserted low, all four power-stage FETs in halfbridges A and B are forced into a high-impedance (Hi-Z) state. Likewise, asserting RESET\_CD low forces all four power-stage FETs in half-bridges C and D into a high-impedance state. Thus, both reset pins are well suited for hard-muting the power stage if needed.

In BTL modes, to accommodate bootstrap charging prior to switching start, asserting the reset inputs low enables weak pulldown of the half-bridge outputs. In the SE mode, the weak pulldowns are not enabled, and it is therefore recommended to ensure bootstrap capacitor charging by providing a low pulse on the PWM inputs when reset is asserted high.

Asserting either reset input low removes any fault information to be signaled on the SD output, i.e., SD is forced high.

A rising-edge transition on either reset input allows the device to resume operation after an overload fault. 

## PACKAGING INFORMATION

Orderable Device	Status <sup>(1)</sup>	Package Type	Package Drawing	Pins	Package Qty	e Eco Plan <sup>(2)</sup>	Lead/Ball Finish	MSL Peak Temp <sup>(3)</sup>
TAS5162DDV	ACTIVE	HTSSOP	DDV	44	35	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-3-260C-168 HR
TAS5162DDVG4	ACTIVE	HTSSOP	DDV	44	35	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-3-260C-168 HR
TAS5162DDVR	ACTIVE	HTSSOP	DDV	44	2000	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-3-260C-168 HR
TAS5162DDVRG4	ACTIVE	HTSSOP	DDV	44	2000	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-3-260C-168 HR
TAS5162DKD	ACTIVE	SSOP	DKD	36	29	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-4-260C-72 HR
TAS5162DKDG4	ACTIVE	SSOP	DKD	36	29	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-4-260C-72 HR
TAS5162DKDR	ACTIVE	SSOP	DKD	36	500	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-4-260C-72 HR
TAS5162DKDRG4	ACTIVE	SSOP	DKD	36	500	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-4-260C-72 HR

<sup>(1)</sup> The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.

**OBSOLETE:** TI has discontinued the production of the device.

(2) Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check http://www.ti.com/productcontent for the latest availability information and additional product content details. TBD: The Pb-Free/Green conversion plan has not been defined.

**Pb-Free (RoHS):** TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes.

**Pb-Free (RoHS Exempt):** This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.

Green (RoHS & no Sb/Br): TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)

<sup>(3)</sup> MSL, Peak Temp. -- The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

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## TAPE AND REEL INFORMATION





## QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



*All dimensions are nominal	*All	dimensions	are	nominal
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Device	Package Type	Package Drawing			Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
TAS5162DDVR	HTSSOP	DDV	44	2000	330.0	24.4	8.6	15.6	1.8	12.0	24.0	Q1



## PACKAGE MATERIALS INFORMATION

27-Jun-2008

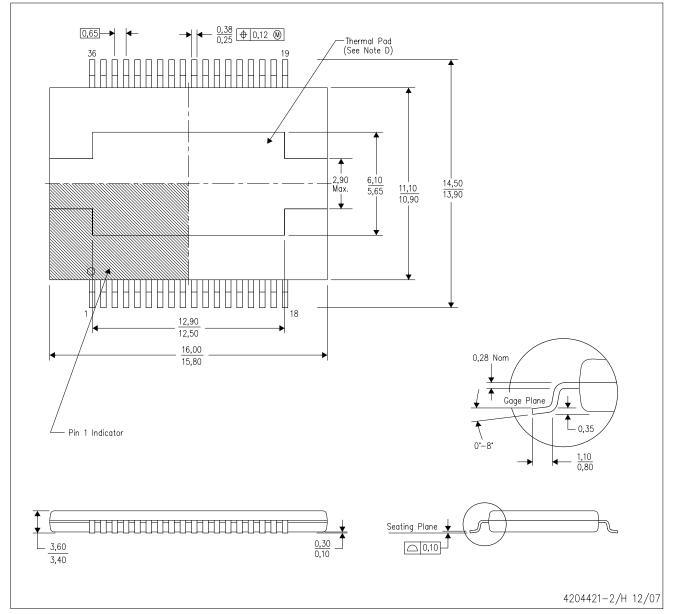


\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
TAS5162DDVR	HTSSOP	DDV	44	2000	346.0	346.0	41.0

DKD (R-PDSO-G36)

PLASTIC SMALL OUTLINE



NOTES: A. All linear dimensions are in millimeters.

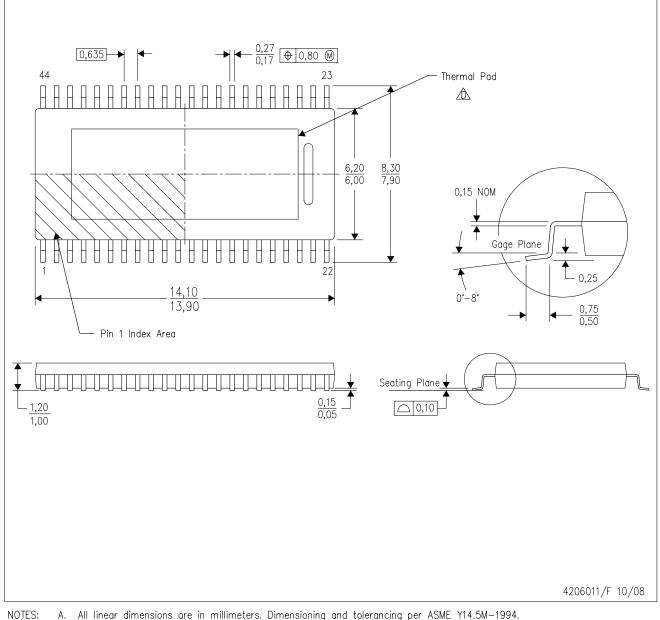
B. This drawing is subject to change without notice.

C. Body dimensions do not include mold flash or protrusion not to exceed 0.15mm.

D. The package thermal performance is optimized for conductive cooling with attachment to an external heat sink. See the product data sheet for details regarding the exposed thermal pad dimensions.



DDV (R-PDSO-G44) PowerPAD<sup>™</sup> PLASTIC SMALL-OUTLINE PACKAGE (DIE DOWN)



B. This drawing is subject to change without notice.

C. Body dimensions do not include mold flash or protrusion not to exceed 0,15.

▲ This package is designed to be attached directly to an external heatsink. Refer to Technical Brief, PowerPad Thermally Enhanced Package, Texas Instruments Literature No. SLMA002 for information regarding recommended board layout. This document is available at www.ti.com <a href="http://www.ti.com">http://www.ti.com</a>. See the product data sheet for details regarding the exposed thermal pad dimensions.

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